



Adaptive sampling with a fleet of autonomous sailing boats using artificial potential fields



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Robotic Sailboats

- Growing activity since ~2006
- Main advantage (and drawback):
 - no need to have embedded power for propulsion
 - autonomy: can be fully autonomous during several days
- Applications
 - Ocean's monitoring
 - Surveillance
 - ...

Robotic Sailboats

Large (more than 2m) sailing robots



(a)



(b)



(c)

(a) Iboat II, ISAE (b) FAST, University of Porto (c) Pinta, University of Aberystwyth (d) Beagle-B, University of Aberystwyth (e) ASV Roboat, INNOC (f) Avalon, ETH Zurich (g) VAIMOS from ENSTA and IFREMER



(d)



(e)



(f)



(g)

Robotic Sailboats

Commercial products



(a)



(b)

- (a) Saildrone (USA),
- (b) Sailbuoy, Offshore sensing AS (No)
- (c) MARS Mayflower Autonomous Research Ship (Project, UK)



(c)

Control architecture

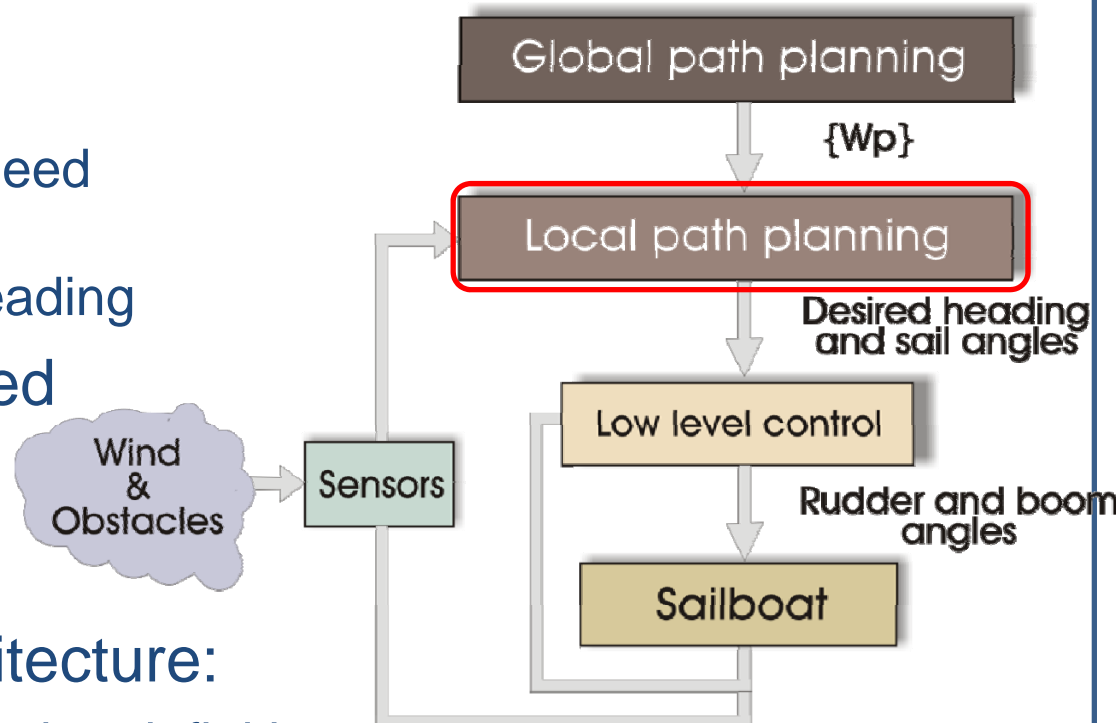
- Control inputs:

- Sail angle
⇒ mainly acts on speed
- Rudder angle
⇒ mainly acts on heading

- Hypothesis: uncoupled

- Layered control architecture:

- High level control: mission definition
- Mid level control: local (**reactive**) path planning
- Low level control



Local path planning

Objectives

- Autonomous navigation of a formation of sailboats to perform adaptive sampling (gradient following,...),
- Dynamic adaptation to environmental conditions (wind, current,...)
- Real-time on-board implementation

Solution

- Potential field based path planning method
- Virtual obstacles for no-go zones constraints

Local path planning

- Use of artificial potential fields method [Khatib87]:
- Principle : $U_t = U_g + \sum U_{ob} + U_{other}$
 - Attractive potential U_g attached to the goal (waypoint)
 - Repulsive potential U_{ob} attached to the obstacles
 - The resulting force (gradient of the potential) drives the robot towards the goal while avoiding obstacles
- Advantages/drawbacks: local
 - Not convenient for dense environment (many obstacles)
 - Can be stuck in local minima
 - **Local** method: numerical evaluation of the gradient in the vicinity of the vehicle
 - ⇒ no need to re-compute the entire path in case of **moving** obstacles or goal

Exo-potential

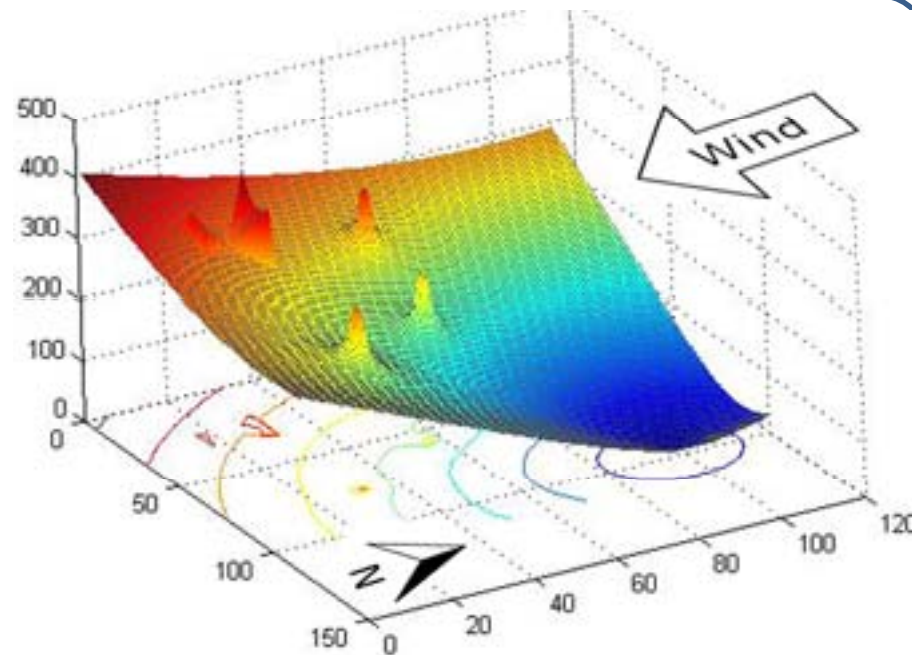
- Attraction to the goal

$$U_g = G_g d_g$$

- Repulsion from the obstacles

$$U_o^{(j)} = G_o \left(\frac{1}{d_o^{(j)}} - \frac{1}{d_{inf}} \right) + G_L \left(\frac{d_{inf} - d_o^{(j)}}{d_{inf}} \right)$$

$$G_L = G_{off} (\mathbf{V} \cdot \mathbf{U} + \|\mathbf{V}\|)$$

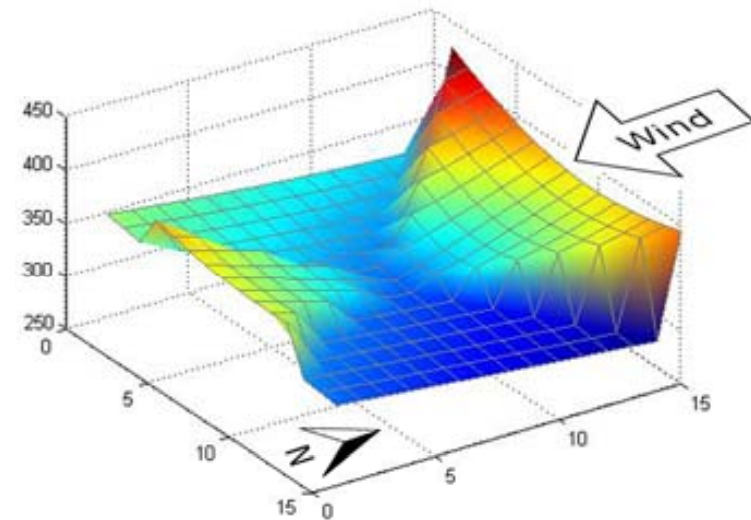
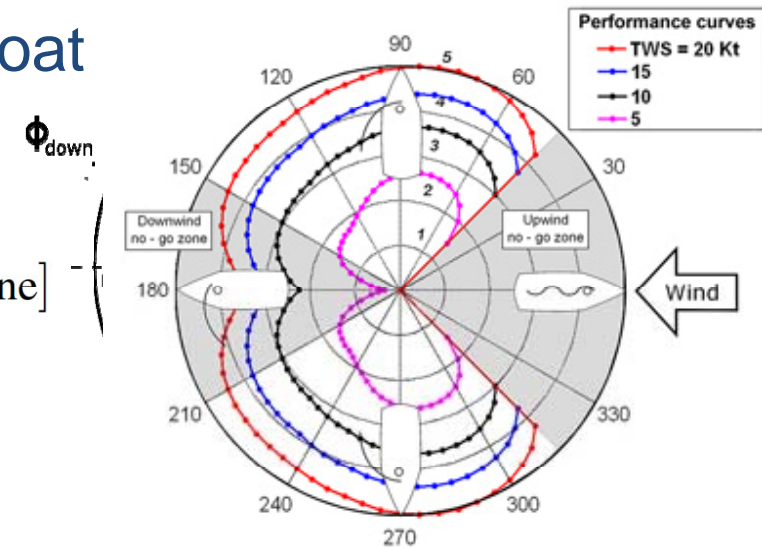


Endo-potential

- Virtual obstacle, moving with the boat
 \Rightarrow Encompass the specific kinematic of the sailboat (speed polar diagram)

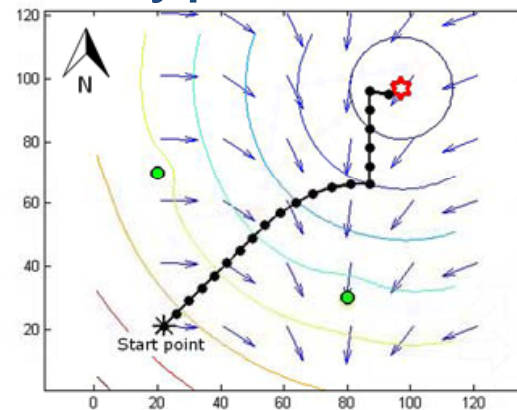
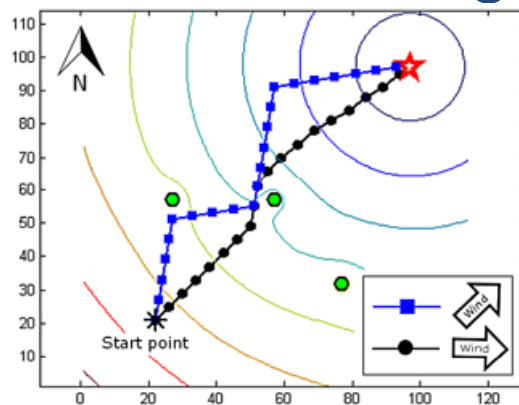
$$U_w = \begin{cases} P_{ngz} & \text{if } \phi \in [\text{no-go zone}] \\ P_h + G_v \frac{V - V_{max}}{V_{max}} & \text{otherwise} \end{cases}$$

- P_h : hysteresis potential to fit the cost of tack and gybe manoeuvres

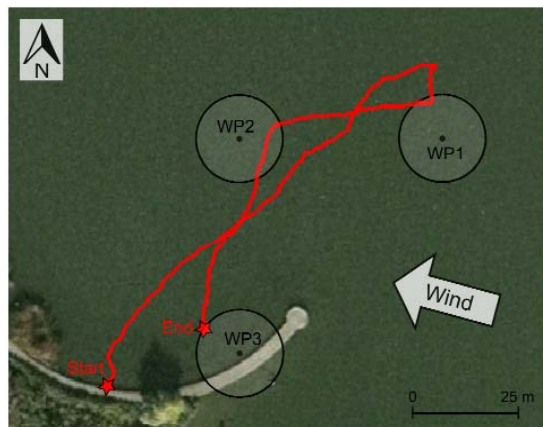


Local path planning

- Classical method: goal = waypoint



Simulation results



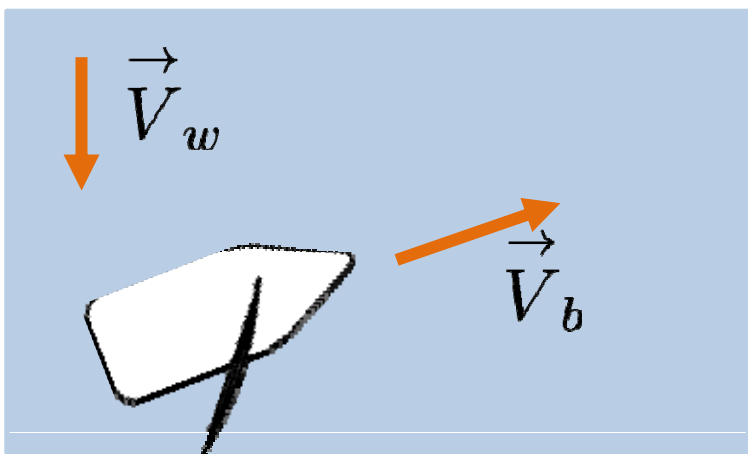
Field trials(Tiny-Sailboat)



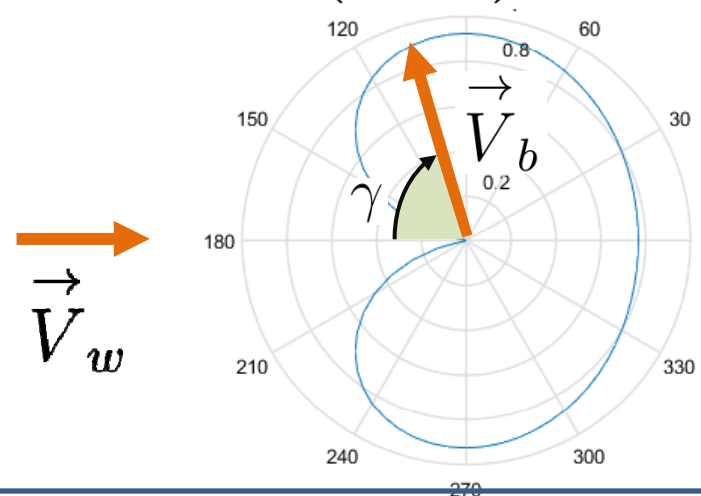
Field trials (Large-Sailboat)

Marine current

- Objective: taking into account the marine current in the local planning
⇒ modify the speed polar diagram
- Hyp.: known current
- Rem. speed polar diagram:



$$\vec{V}_b = P(\vec{V}_w, \gamma)$$



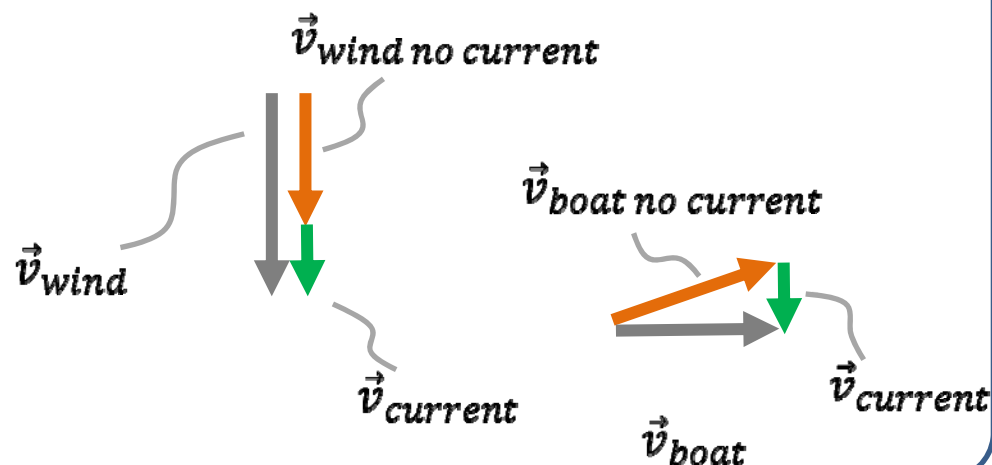
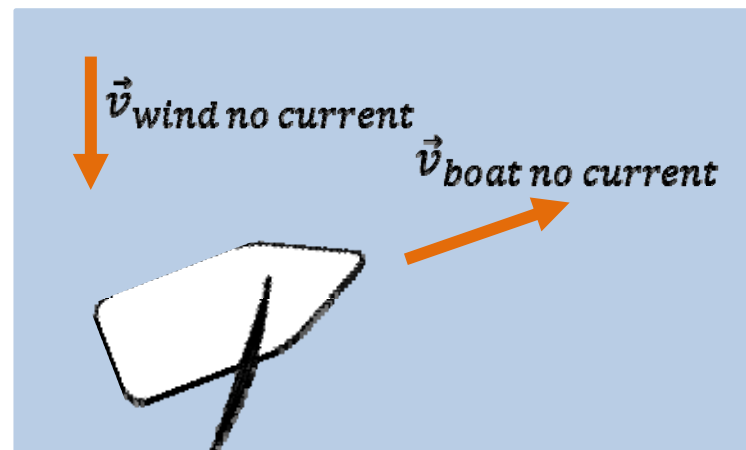
Marine current

- In other words:

$$\vec{V}_b^I = \vec{V}_b^C + \vec{V}_c^I \quad \text{and} \quad \vec{V}_w^I = \vec{V}_w^C + \vec{V}_c^I$$

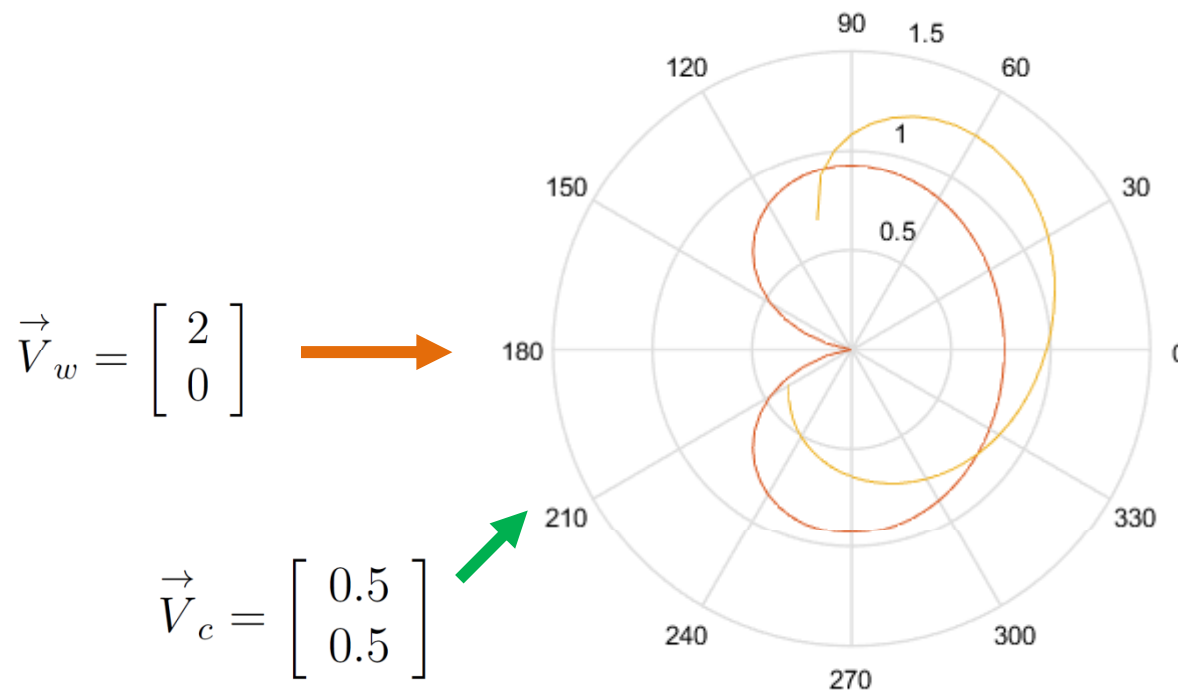
- Speed polar diagram remains usable if both \vec{v}_{current} ↓ vectors are in the same frame:

$$\begin{aligned} \vec{V}_b^I &= \vec{V}_b^C + \vec{V}_c^I \\ &= P\left(\vec{V}_w^C, \gamma\right) + \vec{V}_c^I \\ &= P\left(\vec{V}_w^I - \vec{V}_c^I, \gamma\right) + \vec{V}_c^I \end{aligned}$$



Marine current

- Effects of marine current on the speed polar diagram
 - Translation
 - Distortion



Marine current

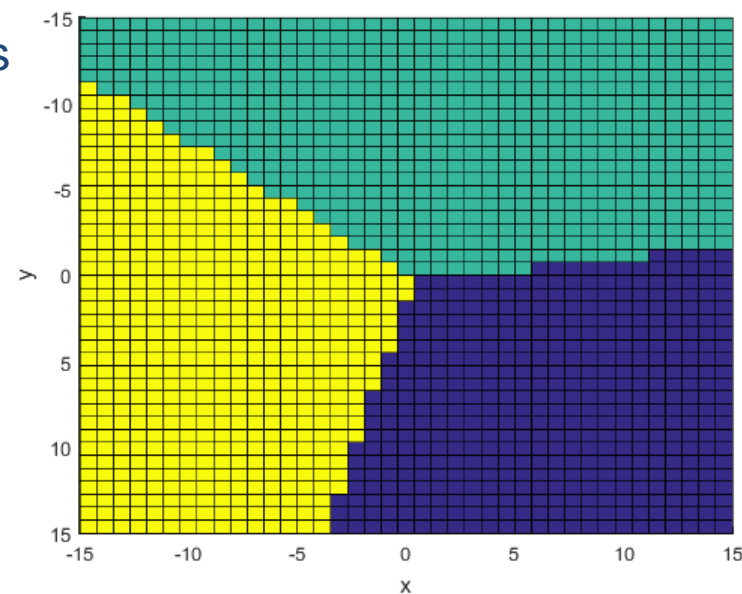
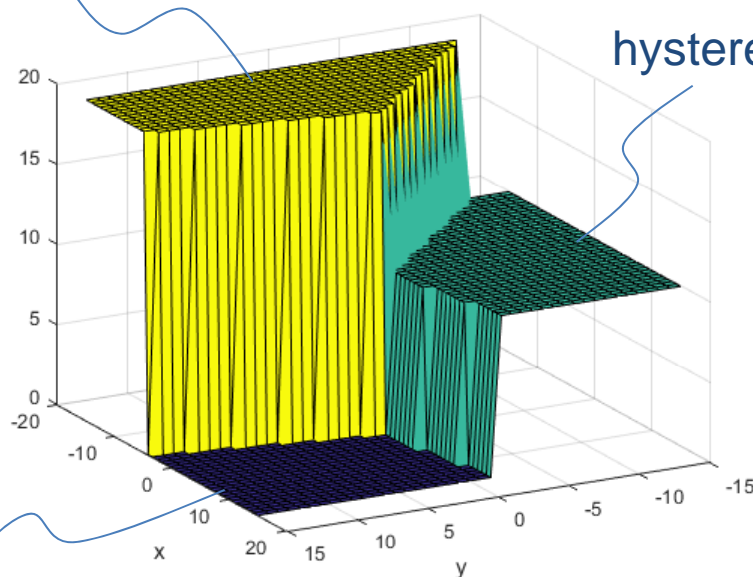
- Wind and current potential fields (endo-potentials)

$$\vec{V}_w = \begin{bmatrix} 2 \\ 0 \end{bmatrix} \quad \vec{V}_c = \begin{bmatrix} 0.5 \\ 0.5 \end{bmatrix}$$

no-go zone

hysteresis

go-zone



- Simulation results

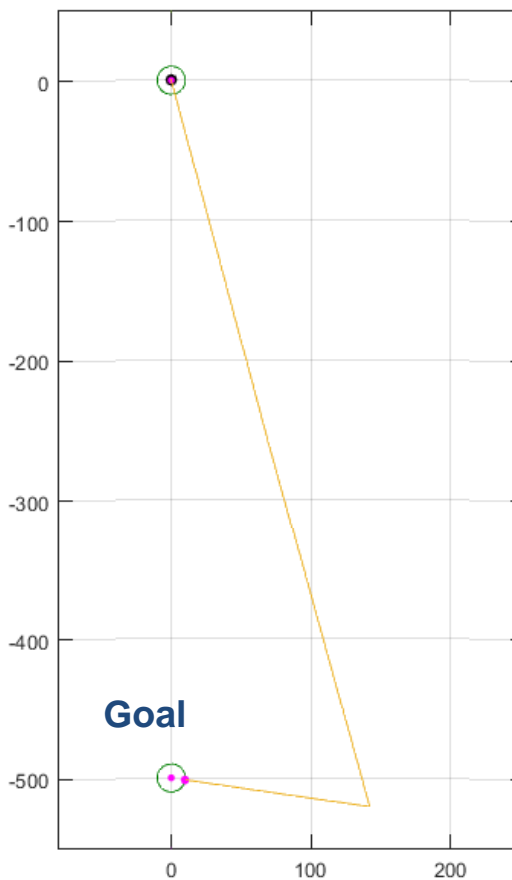
$$\vec{V}_w = \begin{bmatrix} 0 \\ -4 \end{bmatrix}$$

$$\vec{V}_c = \begin{bmatrix} -0.5 \\ 0 \end{bmatrix}$$

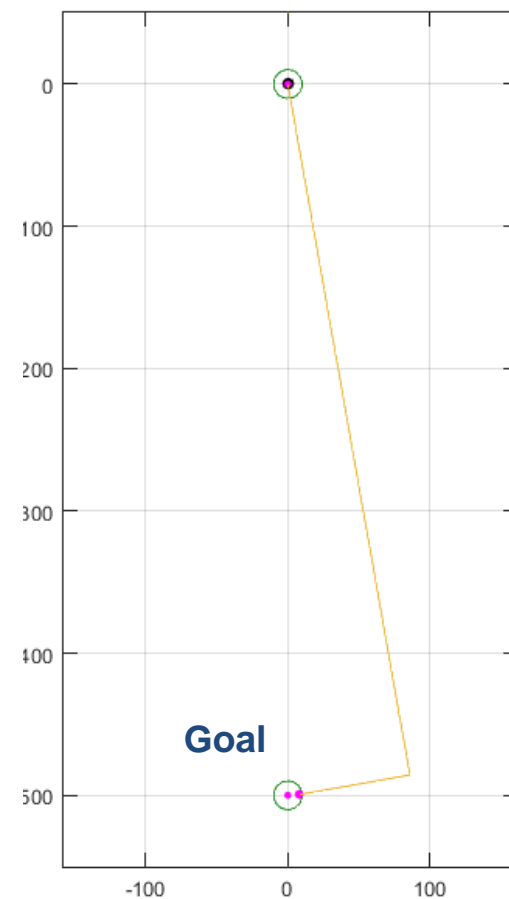
- Cruising time:

- classic PF: 10.8 s
- adapted PF: 9.1 s

Classic PF

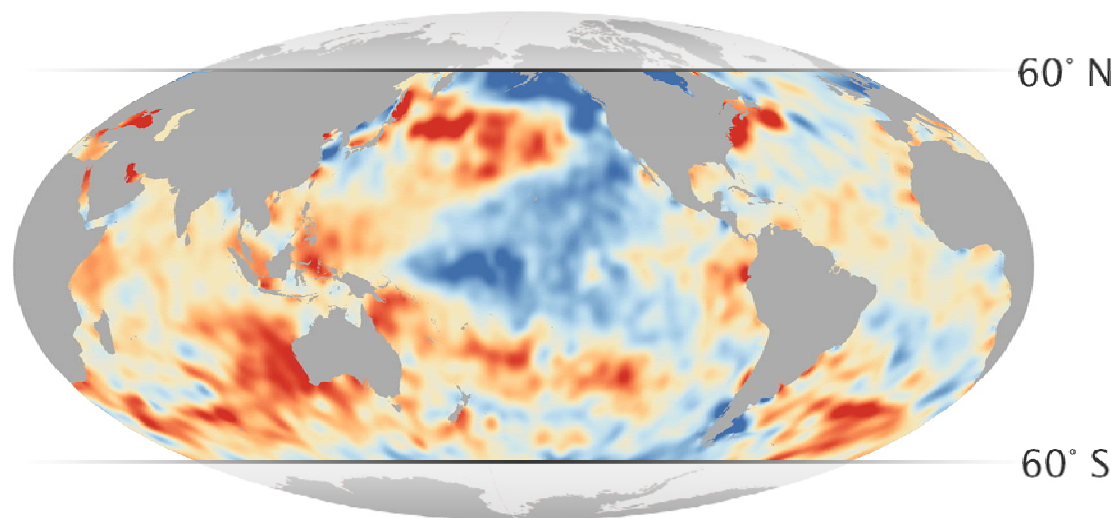


Adapted PF



Formation control

- Motivation: adaptive sampling of the oceans
 - ⇒ following a front or an eddy of some natural field (temperature, salinity, ...)

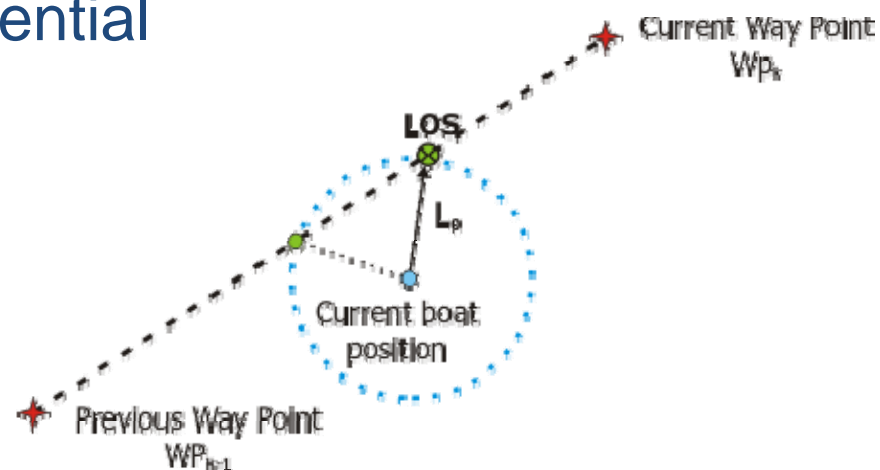


- Move a formation of sailboats in the direction defined by the gradient of the natural field

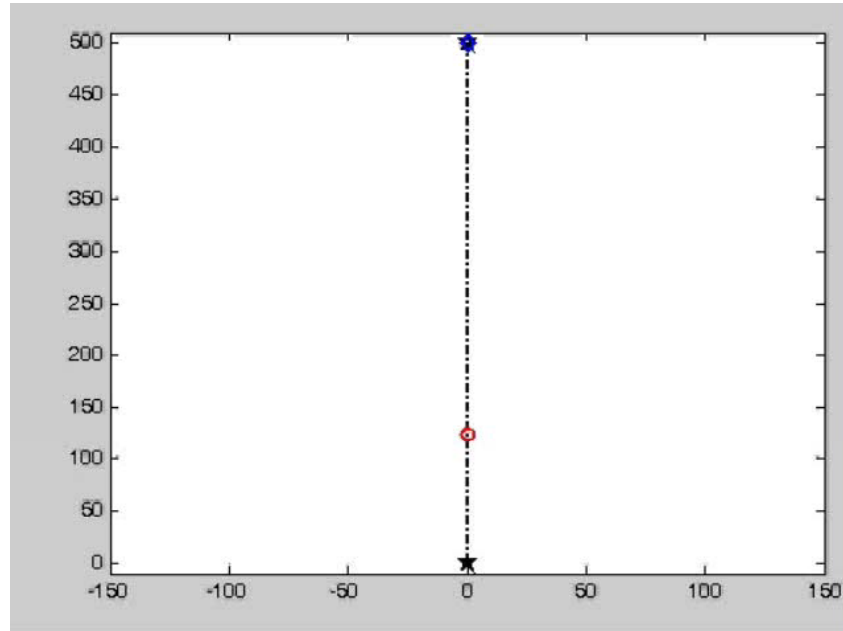
Formation control

- Following a natural gradient fits well within the general framework of the local path planning using (artificial) Potential Fields.
- Remember that PF planning is a **local** method:
Local method: numerical evaluation of the gradient in the vicinity of the vehicle
⇒ no need to re-compute the entire path in case of **moving** goal
- Previous work: use of a moving goal for line following with a sailboat

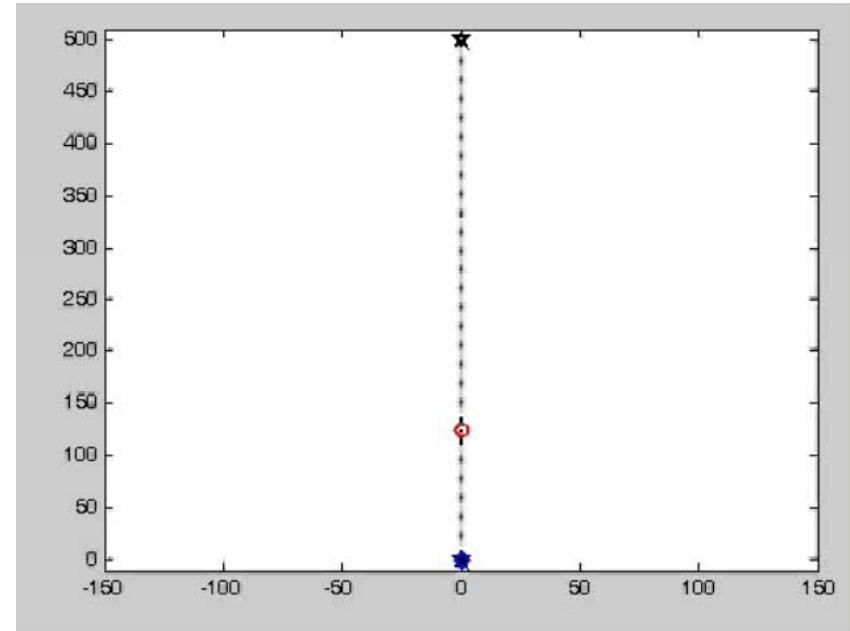
-
- A man wearing a dark green coat and a large black hat is riding a grey donkey. He is carrying a long, thin wooden pole across his shoulders. The background is a rocky, hilly landscape.



Line following : Simulation results



Way point guidance



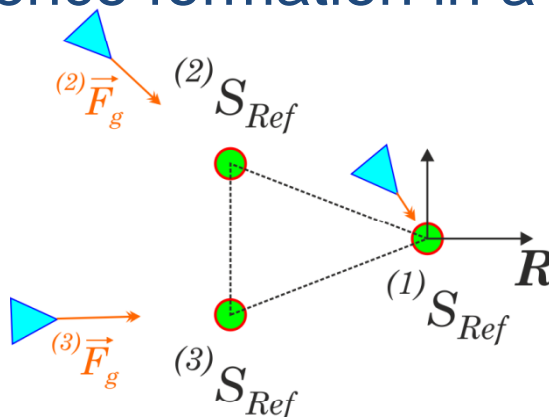
LoS line following

Guaranteed accuracy: less than the LoS length

Formation control

- Define a rigid reference formation in a local frame R

Example with a triangular formation



- Each real vehicle is “linked” to its ref. vehicle in the formation

– For each real vehicle, the resulting force is:

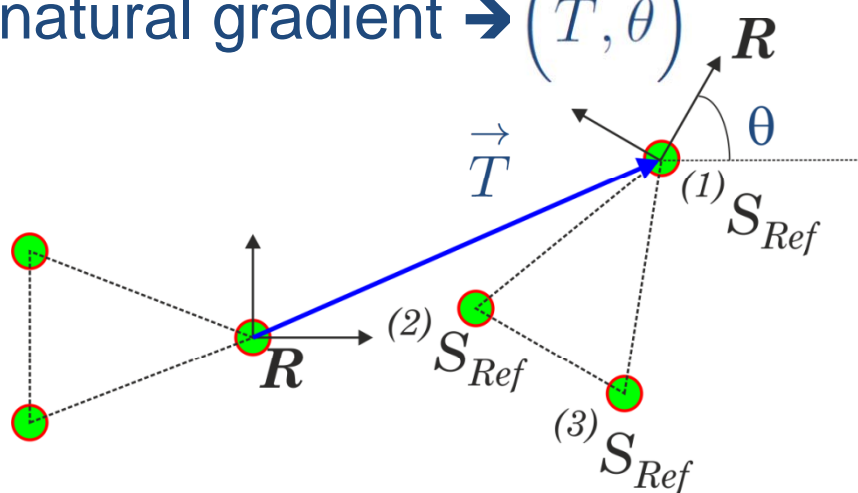
$${}^{(i)}\vec{F} = \vec{grad} \left({}^{(i)}U \right) = {}^{(i)}\vec{F}_g + {}^{(i)}\vec{F}_o + \boxed{{}^{(i)}\vec{F}_w}$$

Including
marine
current

with ${}^{(i)}\vec{F}_g$ = attractive force coming from the (i) ref. vehicle

Formation control

- Drives the reference formation towards the goal (WP) or to follow some natural gradient $\rightarrow (\vec{T}, \theta)$

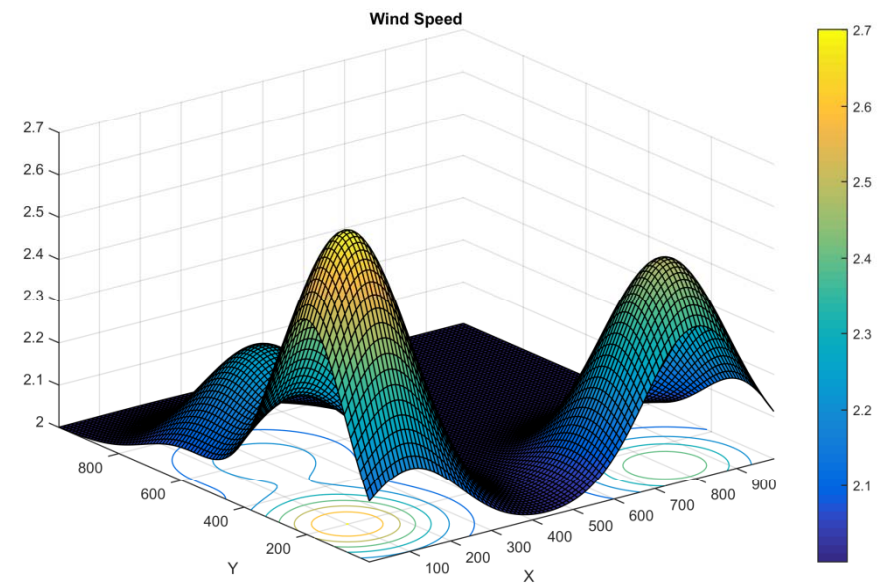
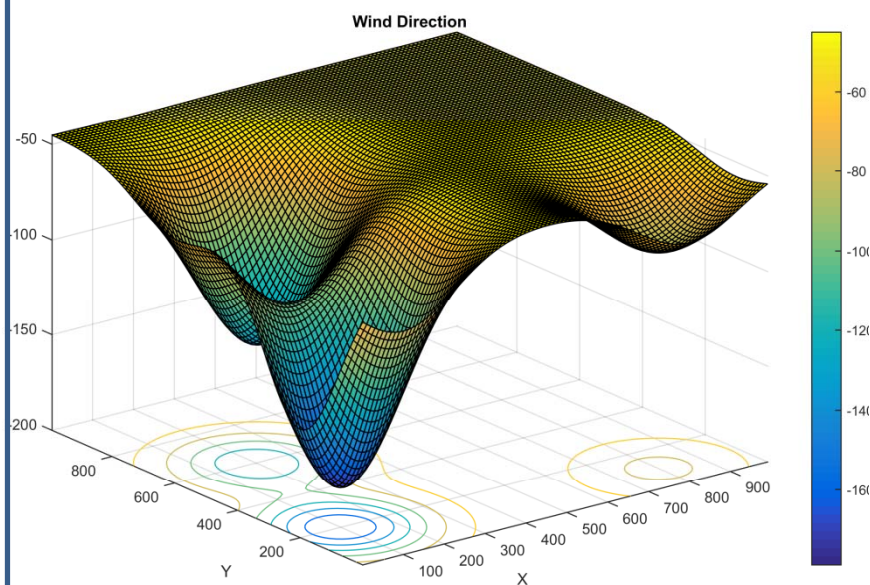


Choice of (\vec{T}, θ)

- Translation : cruise control $|\vec{T}| = V_{max}dt - K_v \overline{dist}$
- Rotation: arbitrary
 - $\theta = 0$: orientation remains constant in a fixed frame
 - θ such that $\overrightarrow{{}^{(2)}S_{Ref} {}^{(3)}S_{Ref}} \perp \vec{T}$: formation is pointing toward the goal

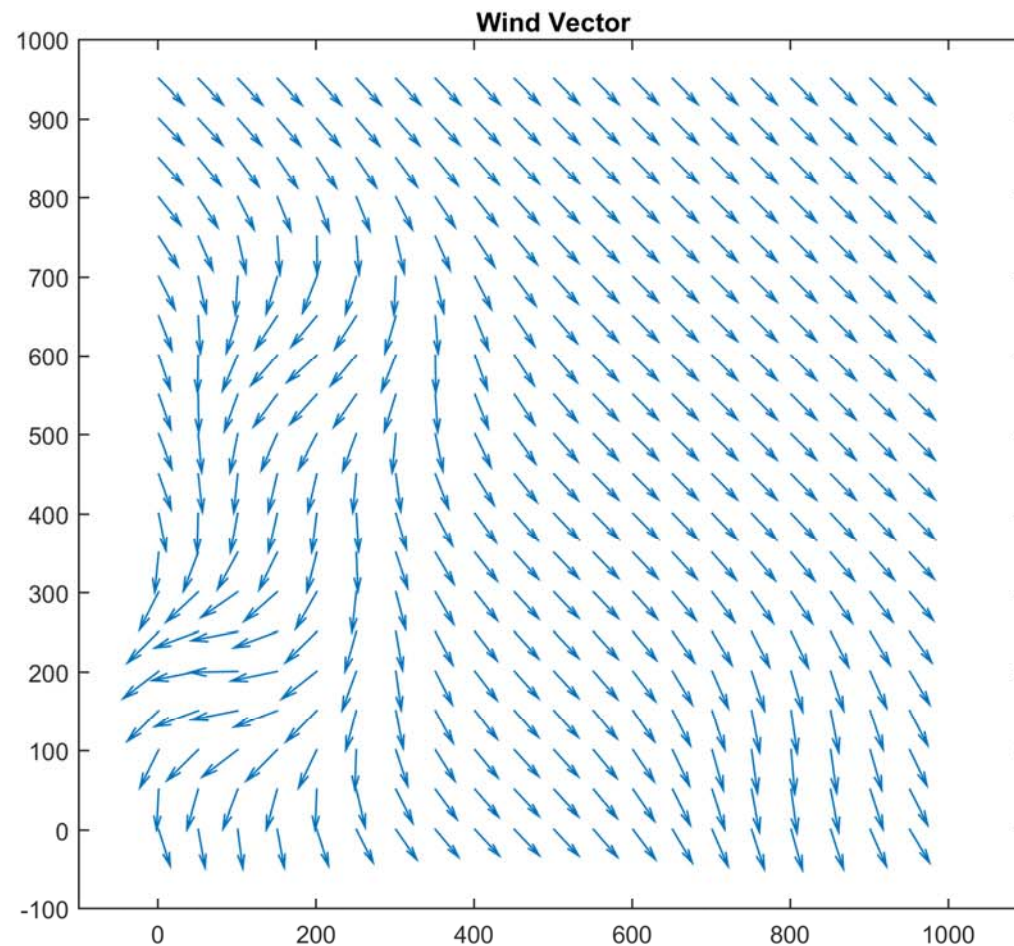
Formation control

- Simulation : reaching a way point (varying wind field)



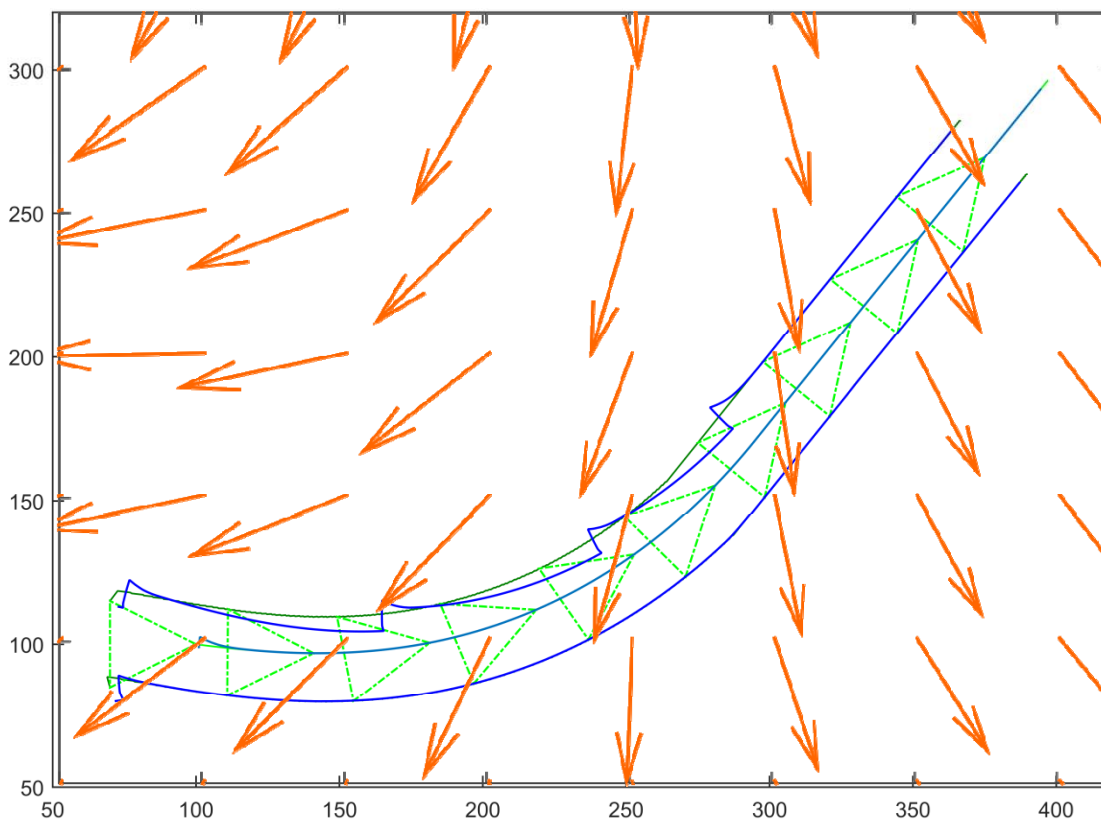
Formation control

- Simulation : reaching a way point (varying wind field)



Formation control

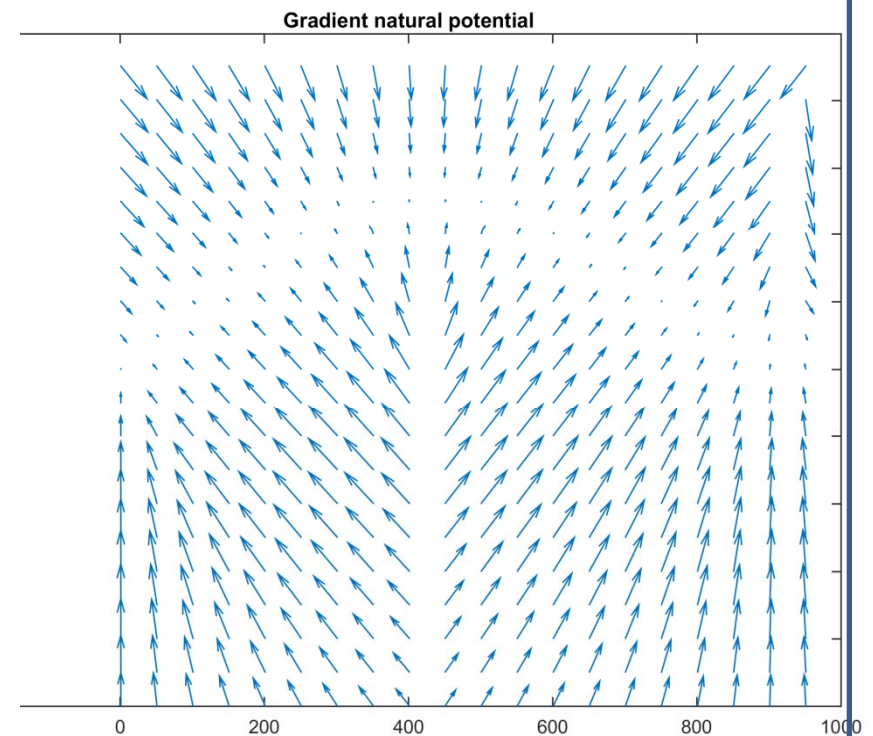
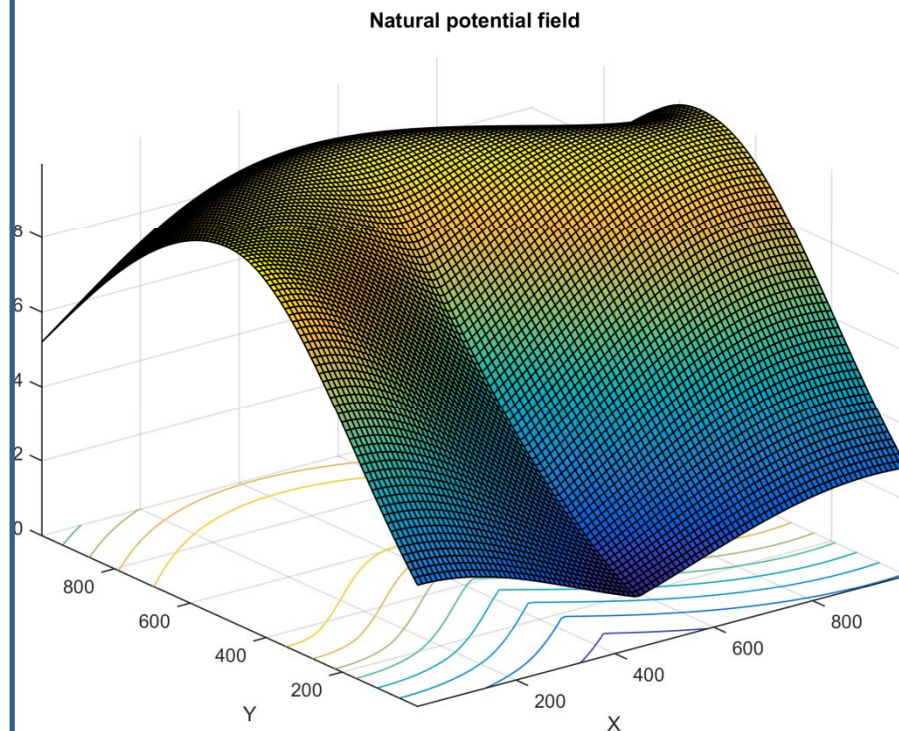
- Simulation : reaching a way point (varying wind field)



Leader-Follower formation
PF planning applied to the
ref. Leader

Formation control

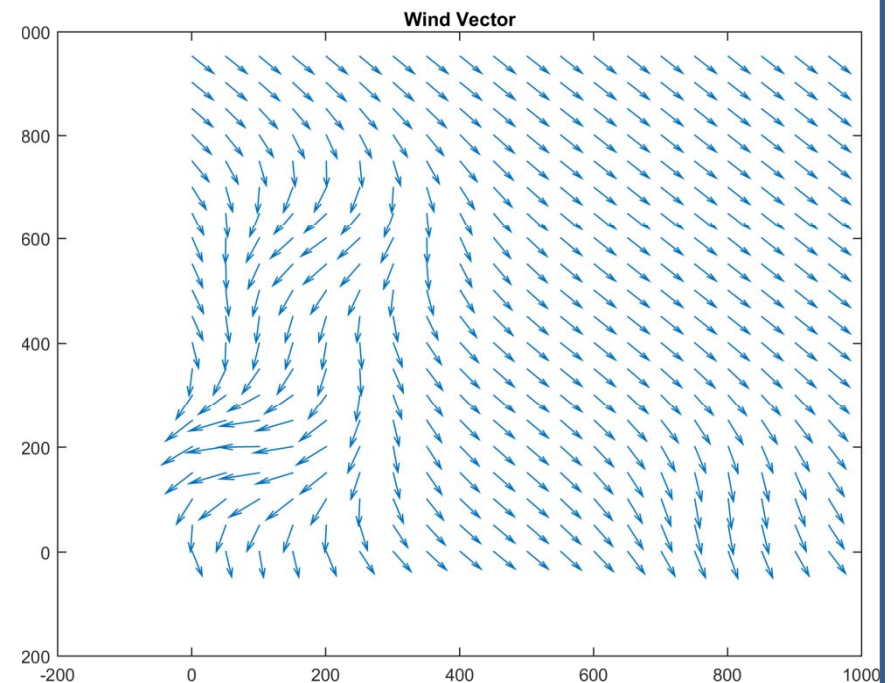
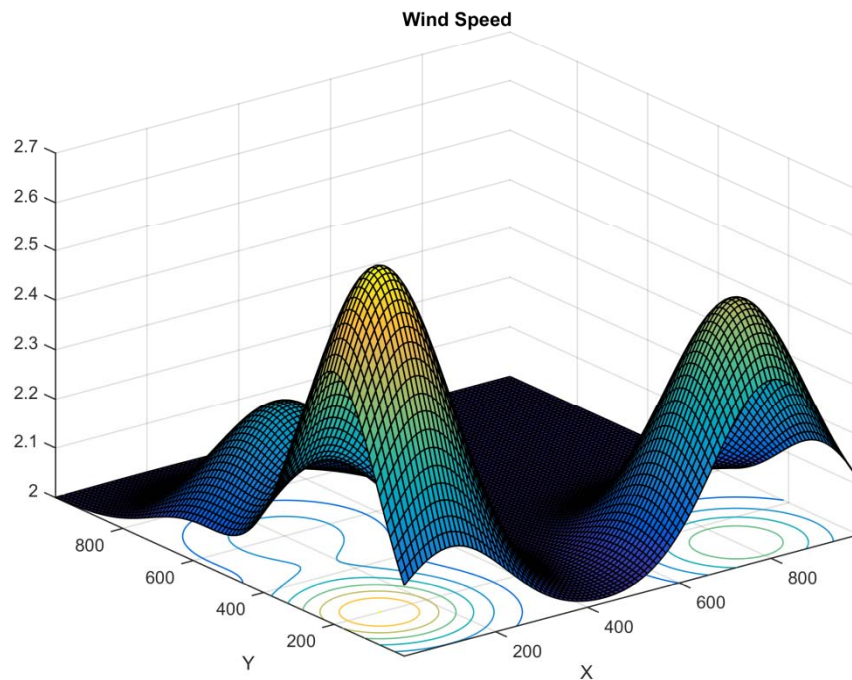
- Simulation : following a natural field gradient (varying wind field)



Natural potential field

Formation control

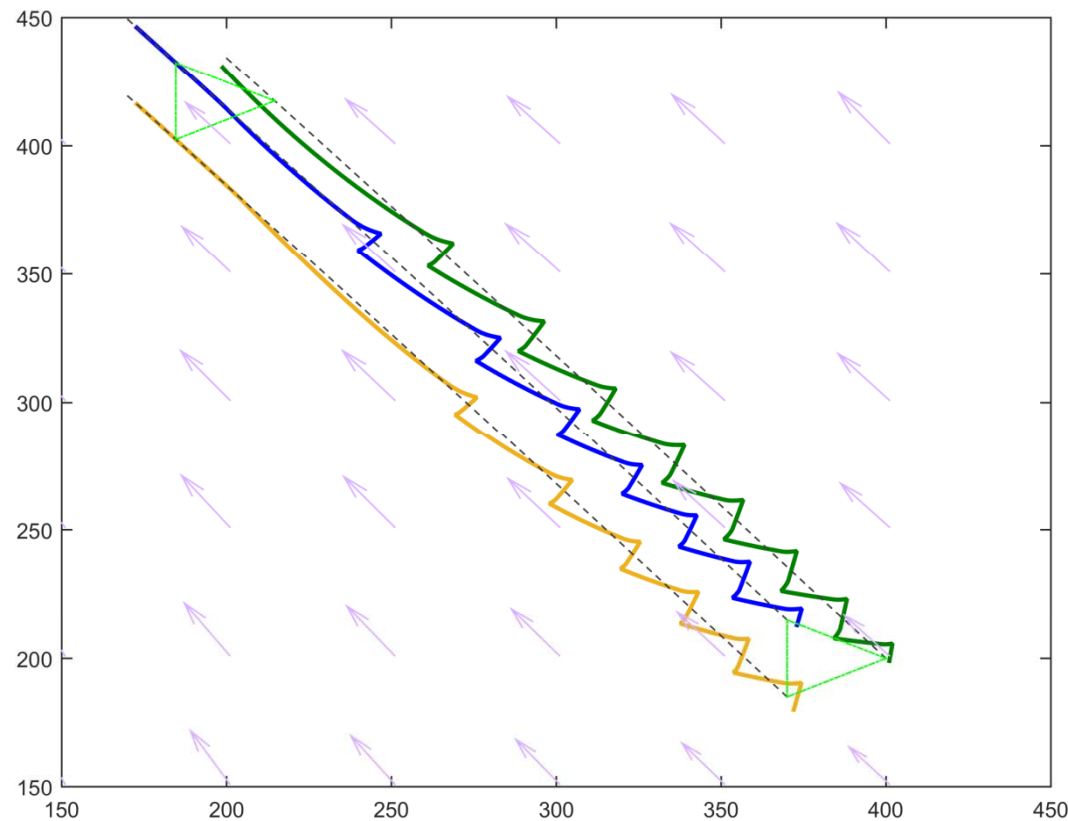
- Simulation : following a natural field gradient (varying wind field)



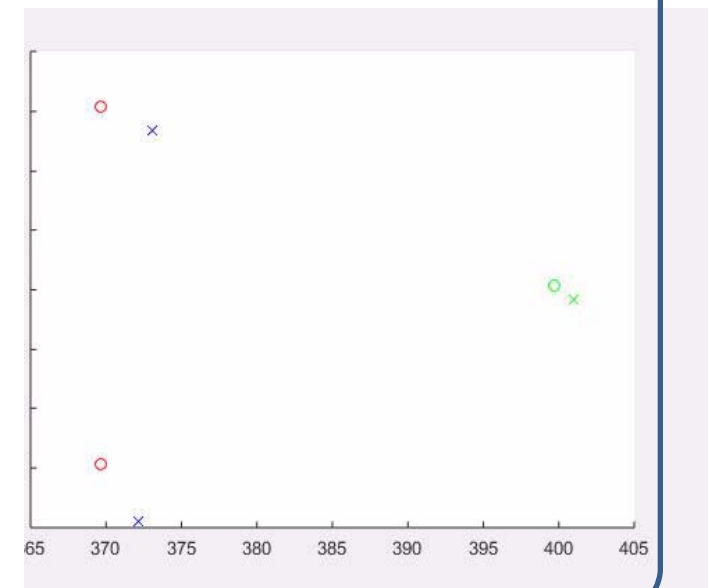
Wind field

Formation control

- Simulation : following a natural field gradient (varying wind field)

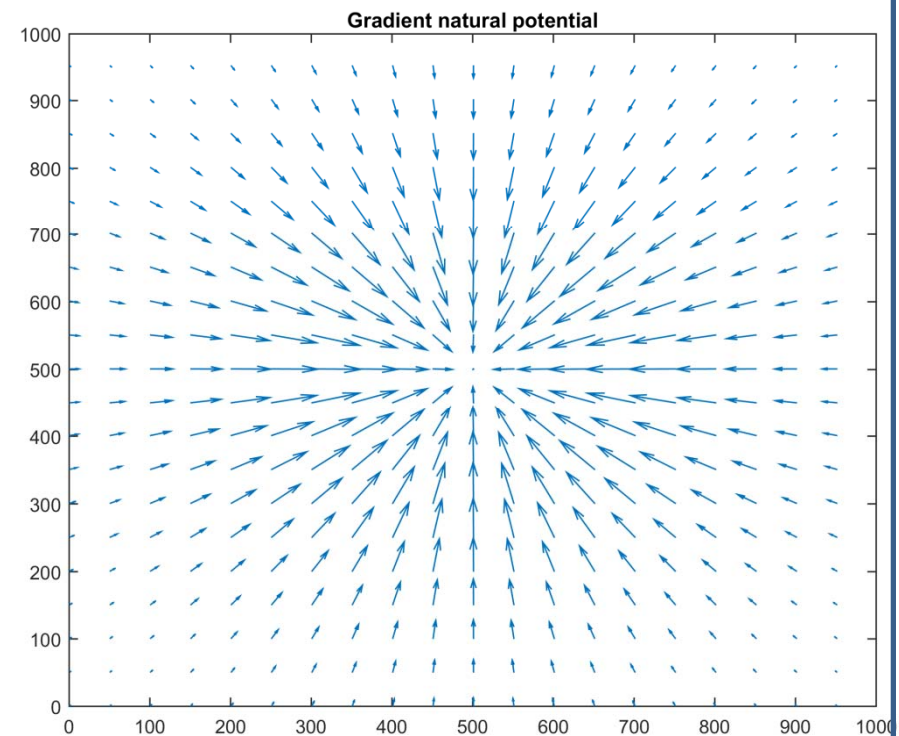
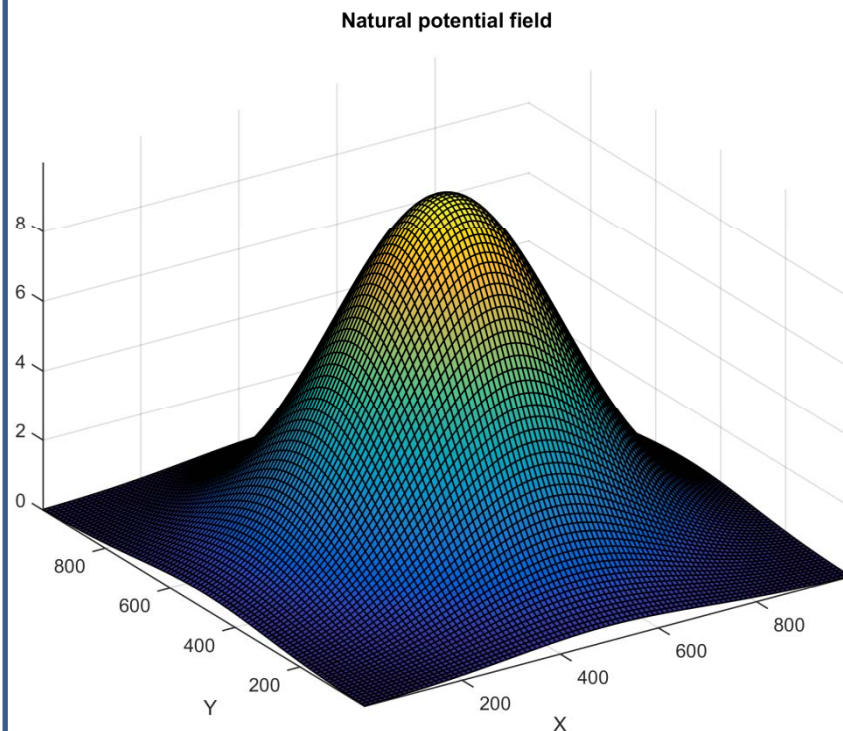


PF planning **not** applied to the ref. formation
Constant orientation in a fixed frame



Formation control

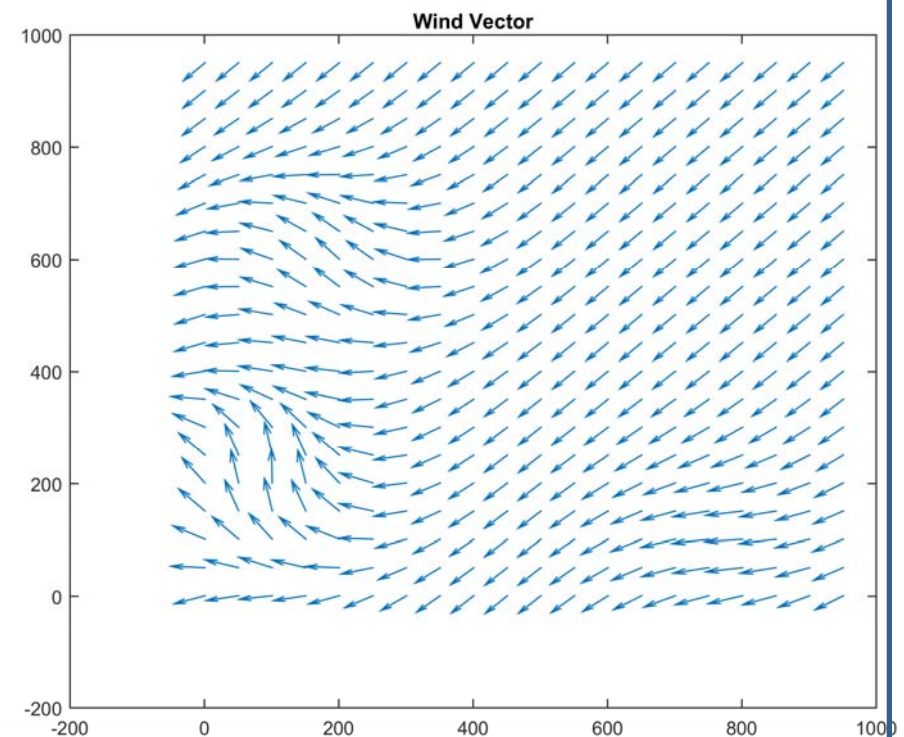
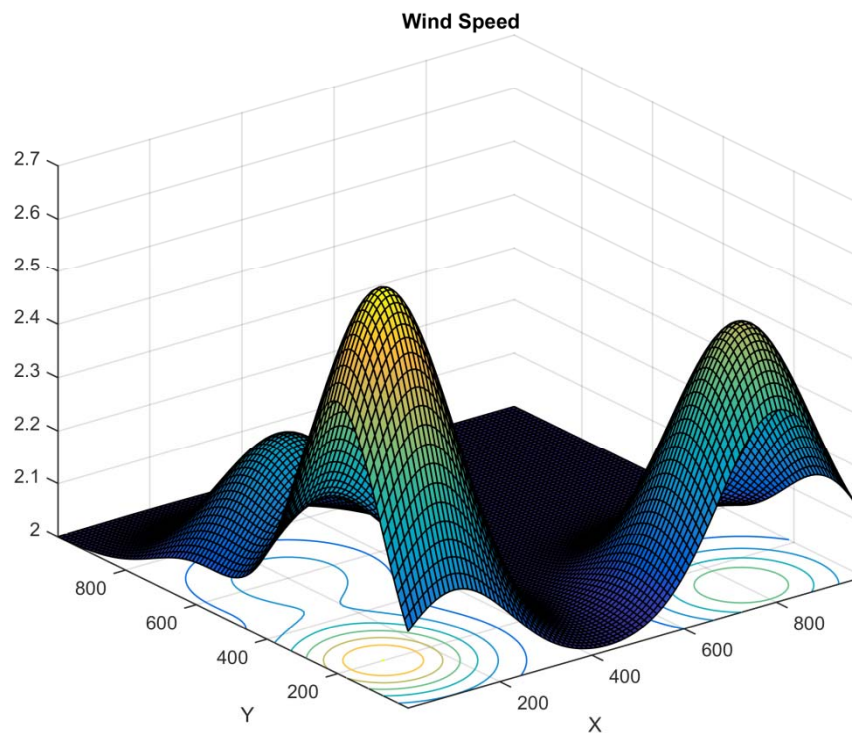
- Simulation : following a natural field gradient then follow an isoline (varying wind field)



Natural potential field

Formation control

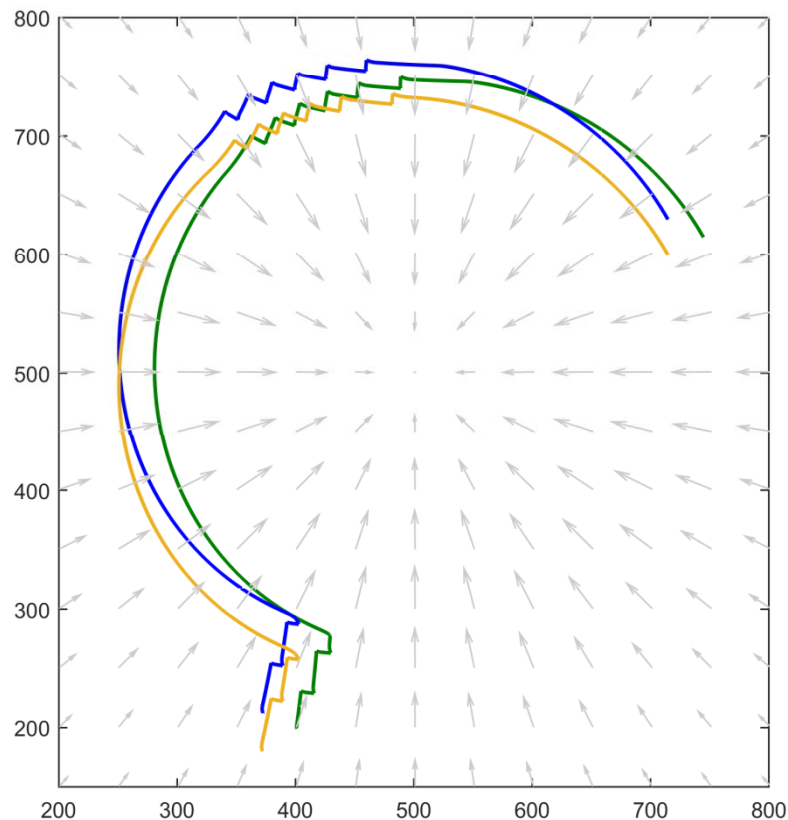
- Simulation : following a natural field gradient then follow an isoline (varying wind field)



Wind field

Formation control

- Simulation : following a natural field gradient then follow an isoline (varying wind field)



PF planning **not** applied to
the ref. formation
Constant orientation in a
fixed frame

Conclusion

Formation control of sailboats for adaptive sampling

⇒ different features (Way point reaching, gradient or isoline following)

Includes wind and marine current

Light code

⇒ Easy on-board implementation

